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# Trailing Edge Noise Prediction Based on a New Acoustic Formulation

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# Outline

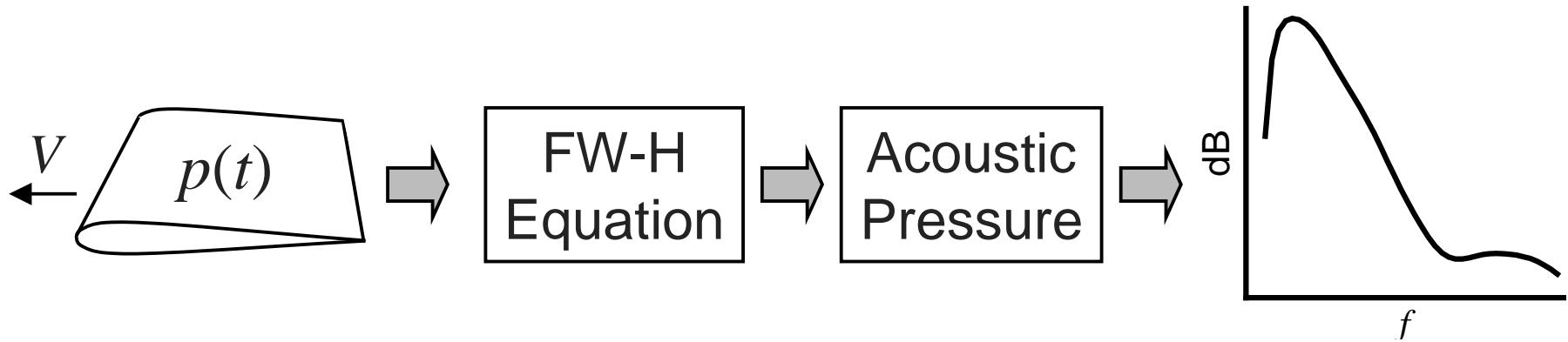
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- Introduction / Motivation
- Acoustic Formulation
- Model Problems – Constant Frequency
  - Surface Pressure from Thin Airfoil Theory
  - Velocity Scaling Properties, Directivity
- Broadband Noise Prediction
  - Trailing Edge Noise
  - Surface Pressure Formulation
    - (Schlinker and Amiet, 1981)
  - Comparison with Experiment
    - (Brooks and Hodgson, 1981)



# Introduction / Motivation

- Broadband Noise Prediction Tools
  - Airframe noise, ducted fan noise
  - Incident turbulence, TE noise
- Time Domain Approach
  - Acoustic Analogy
  - Ffowcs Williams – Hawkings equation
  - Decouples aerodynamics from acoustics
  - Input from CFD or experiment

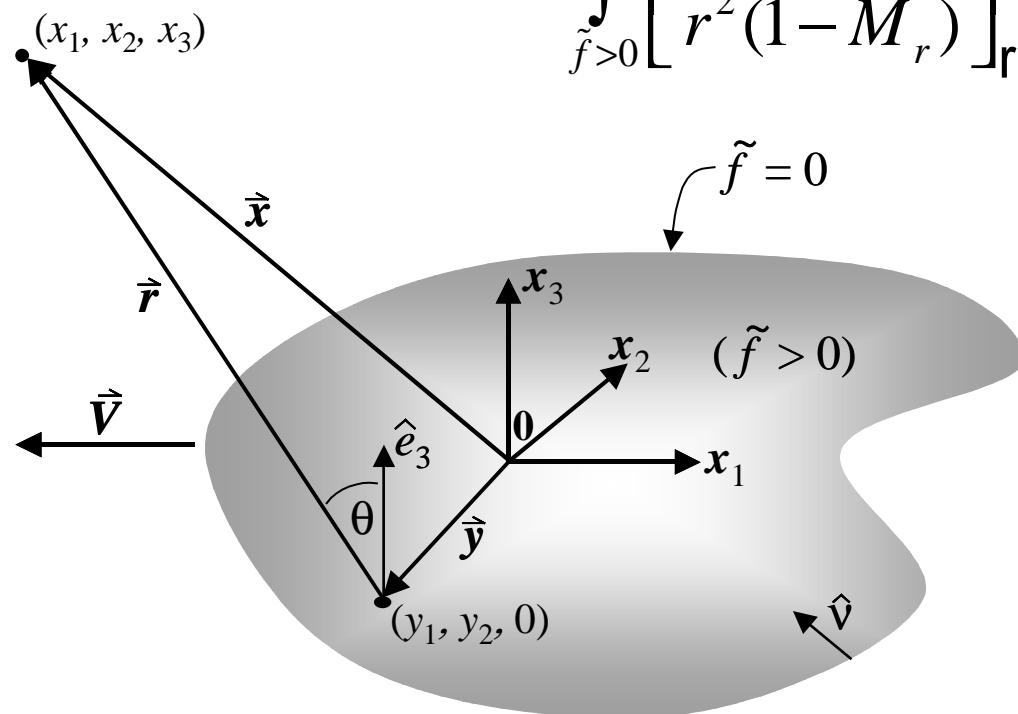




# Formulation 1B

$$4\pi p'(\vec{x}, t) = \int_{\tilde{f} > 0} \left[ \frac{(\partial p / \partial \tau - V \partial p / \partial s) \cos \theta}{c_0 r (1 - M_r)} \right]_{\text{ret}} dS$$

$$+ \int_{\tilde{f} > 0} \left[ \frac{p \cos \theta}{r^2 (1 - M_r)} \right]_{\text{ret}} dS - \int_{\tilde{f} = 0} \left[ \frac{M_v p \cos \theta}{r (1 - M_r)} \right]_{\text{ret}} d\ell$$





# Model Problems

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## Test Cases

- Directivity
- Velocity Scaling Properties

## Analytic Surface Pressure

- Thin Airfoil Theory (Amiet, 1975-6)
- Constant Frequency Disturbance
- Flat Plate in Uniform Rectilinear Motion



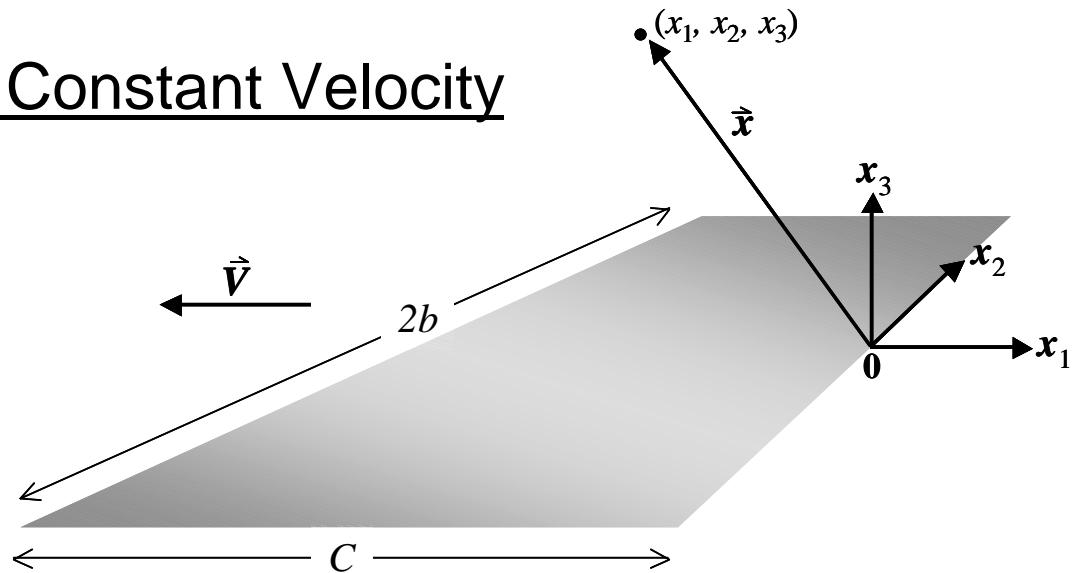
# Analytic Surface Pressure

## Rectangular Surface at Constant Velocity

$$-C \leq x_1 \leq 0,$$

$$-b \leq x_2 \leq b,$$

$$\vec{V} = [-U, 0, 0]^T$$



## Surface pressure

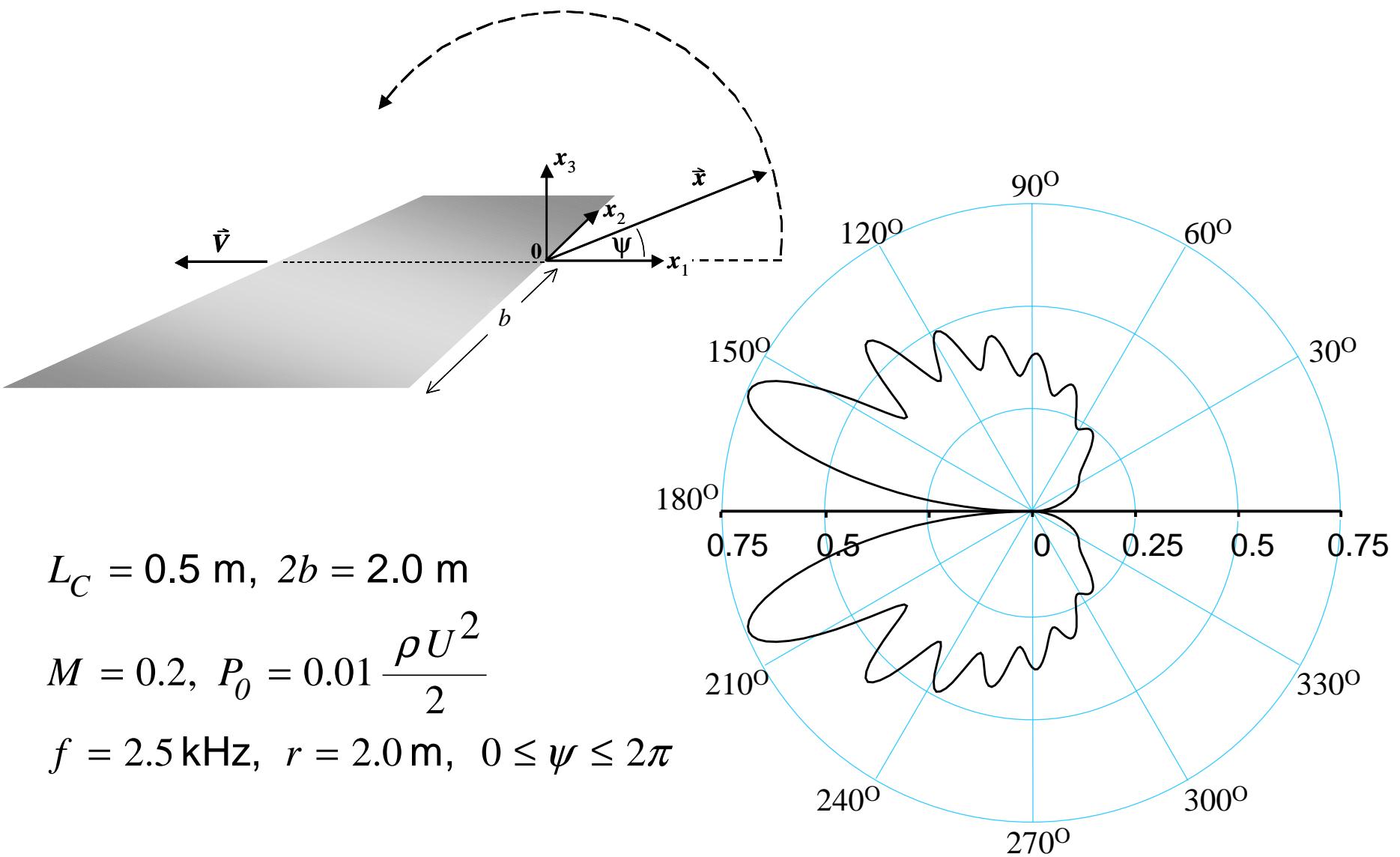
$$\Delta P(x_1, t) = 2P_0 g(x_1, k_c) e^{-ik_c(x_1 - Ut)}$$

$$k_c = \omega/U_c = \text{constant}$$

$g(x_1, k_c)$  from thin airfoil theory (Amiet, 1975)

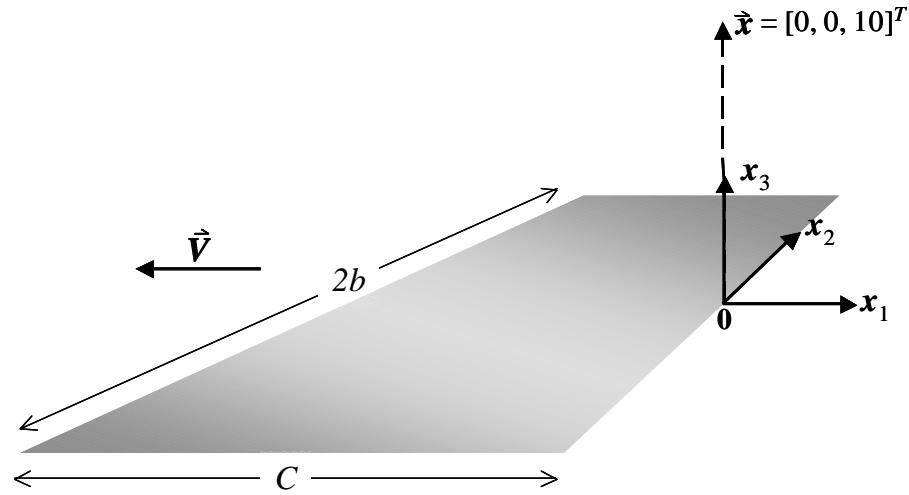


# Directivity





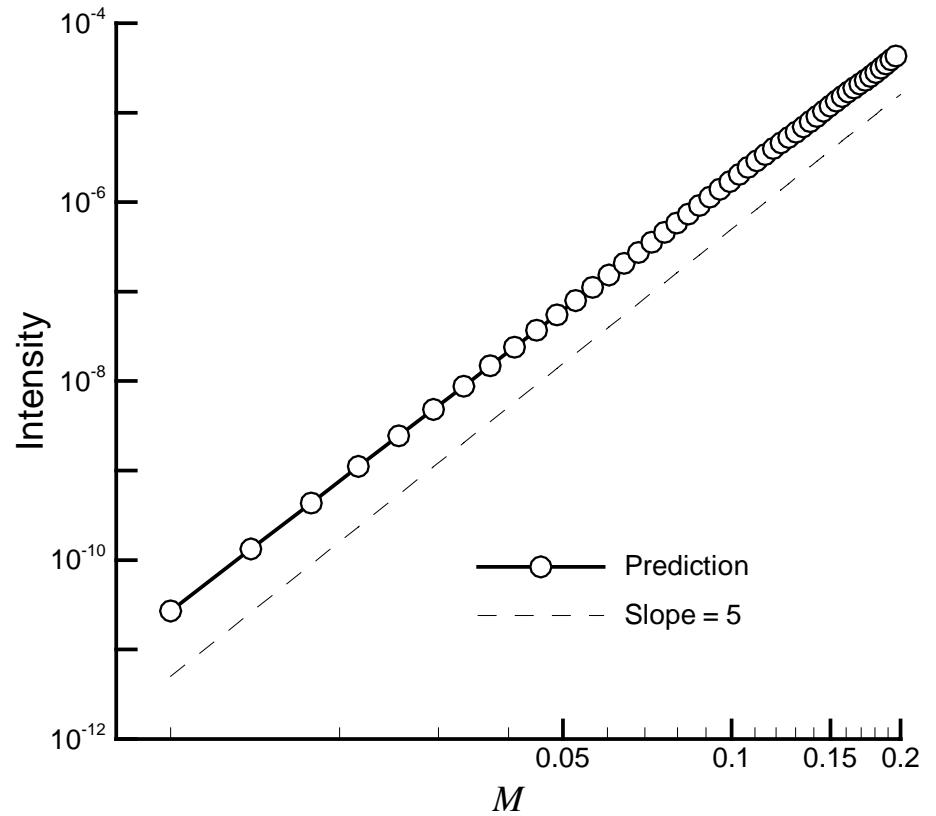
# Velocity Scaling



$$L_C = 0.5 \text{ m}, \quad 2b = 2.0 \text{ m}$$

$$0.01 \leq M \leq 0.2, \quad P_0 = 0.01 \frac{\rho U^2}{2}$$

$$f = 2.5 \text{ kHz}, \quad r = 10 \text{ m}, \quad \psi = 0$$





# Broadband Trailing Edge Noise

Experiment: Brooks and Hodgson (1981)

NACA 0012 Airfoil

Chord = 0.61 m

Span = 0.46 m

$\alpha$  = 0 degrees

Tunnel Speeds

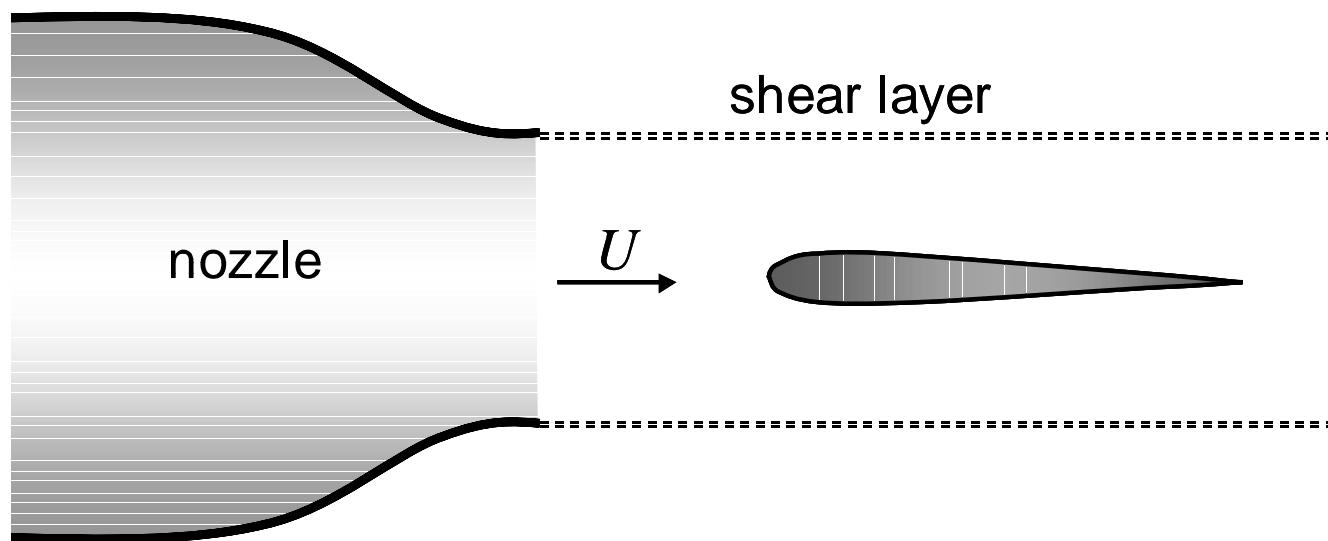
$U$  = 38.6 m/s

$U$  = 69.5 m/s

Microphone

$r$  = 1.22 m

$\theta$  = 90 degrees





# Broadband Surface Pressure

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Broadband extension:

$$\Delta P(x_1, x_2, t) =$$

$$2 \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \tilde{P}(k_c, k_2) g(x_1, k_c, k_2) e^{-i [k_c(x_1 - U_c t) + k_2 x_2]} dk_c dk_2$$

For acoustic prediction:

$$\Delta P(x_1, x_2, t) = 2\pi \int_{-\infty}^{\infty} \tilde{P}(k_c, 0) g(x_1, k_c, 0) e^{-i k_c (x_1 - U_c t)} dk_c$$



# Broadband Surface Pressure

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Stochastic model:

$$\Delta P(x_1, t) \approx 2\pi \sum_{n=-N}^N A_{n,0} e^{i\varphi_n} g(x, k_{c,n}, 0) e^{-ik_{c,n}(x_1 - U_c t)}$$

$$A_{n,0} = [\Phi_{PP}(k_{c,n}, 0) \Delta k_c]^{1/2}$$

$\Phi_{PP}(k_c, k_2)$  = PSD of surface pressure

$\varphi_n$  = random phase angle on  $[0, 2\pi]$



# Surface Pressure PSD

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Schlinker and Amiet (1981)

$$\Phi_{PP}(k_c, 0) = \frac{U_c}{\pi} \ell_2(\omega) S_{qq}(\omega, 0)$$

$\ell_2(\omega)$  = spanwise correlation length

$S_{qq}(\omega, \Delta x_2)$  = surface pressure correlation function

First-Cut Prediction:

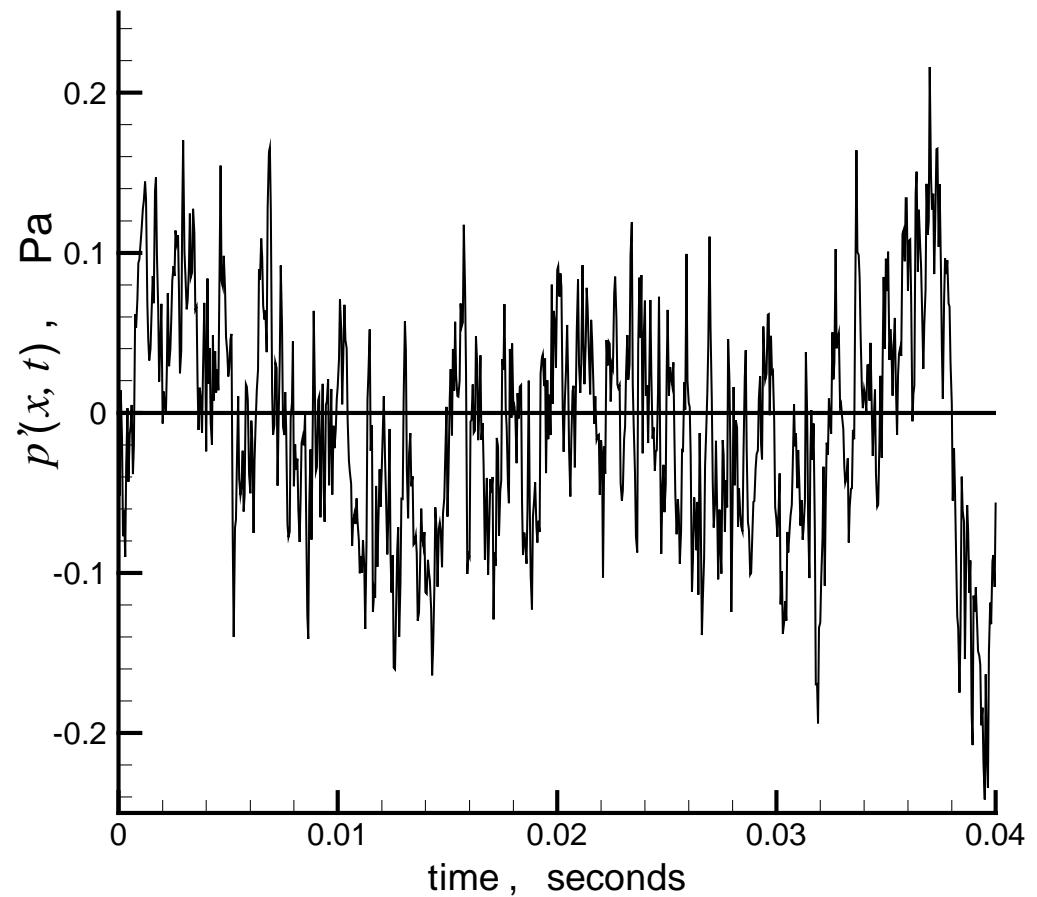
Evaluate  $\ell_2(\omega)$  and  $S_{qq}(\omega, 0)$  by empirically determined flat plate formulations.



# Broadband Prediction in Time

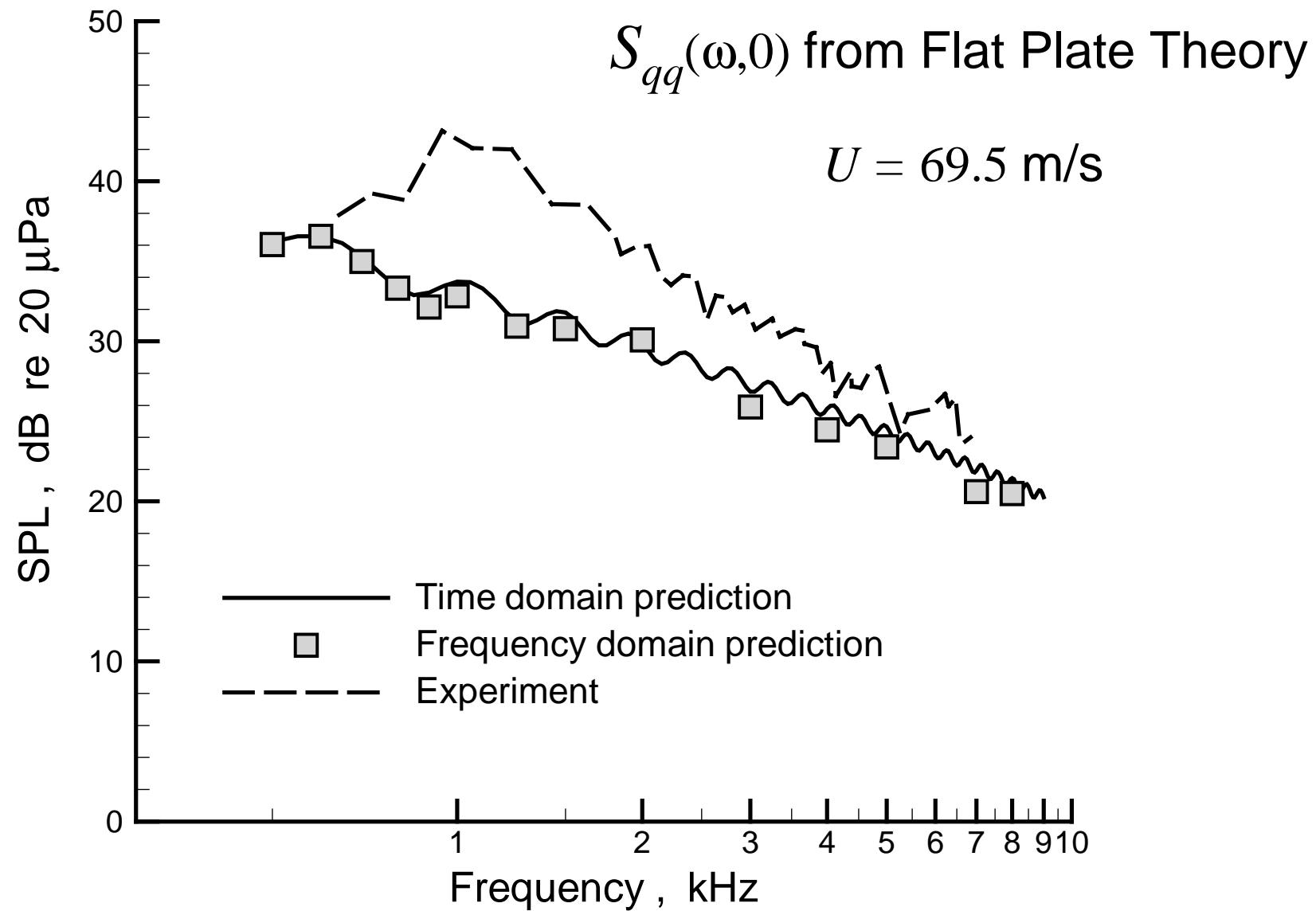
- Surface pressure input to Formulation 1B
- $25 \text{ Hz} < f < 10 \text{ kHz}$
- Acoustic pressure Fourier analyzed to convert to narrowband SPL

Predicted Signal  
 $U = 69.5 \text{ m/s}$



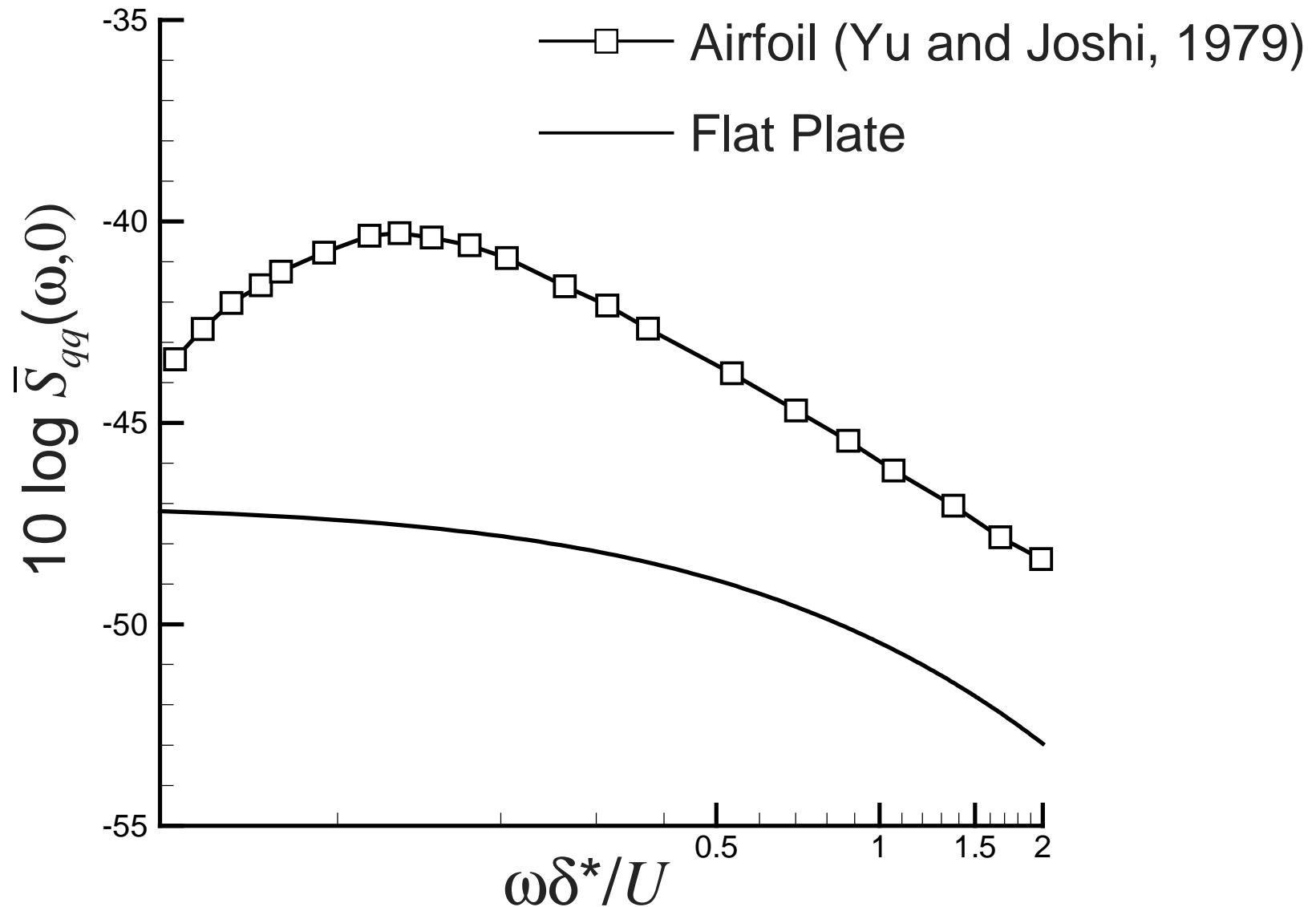


# Far Field Noise Spectrum



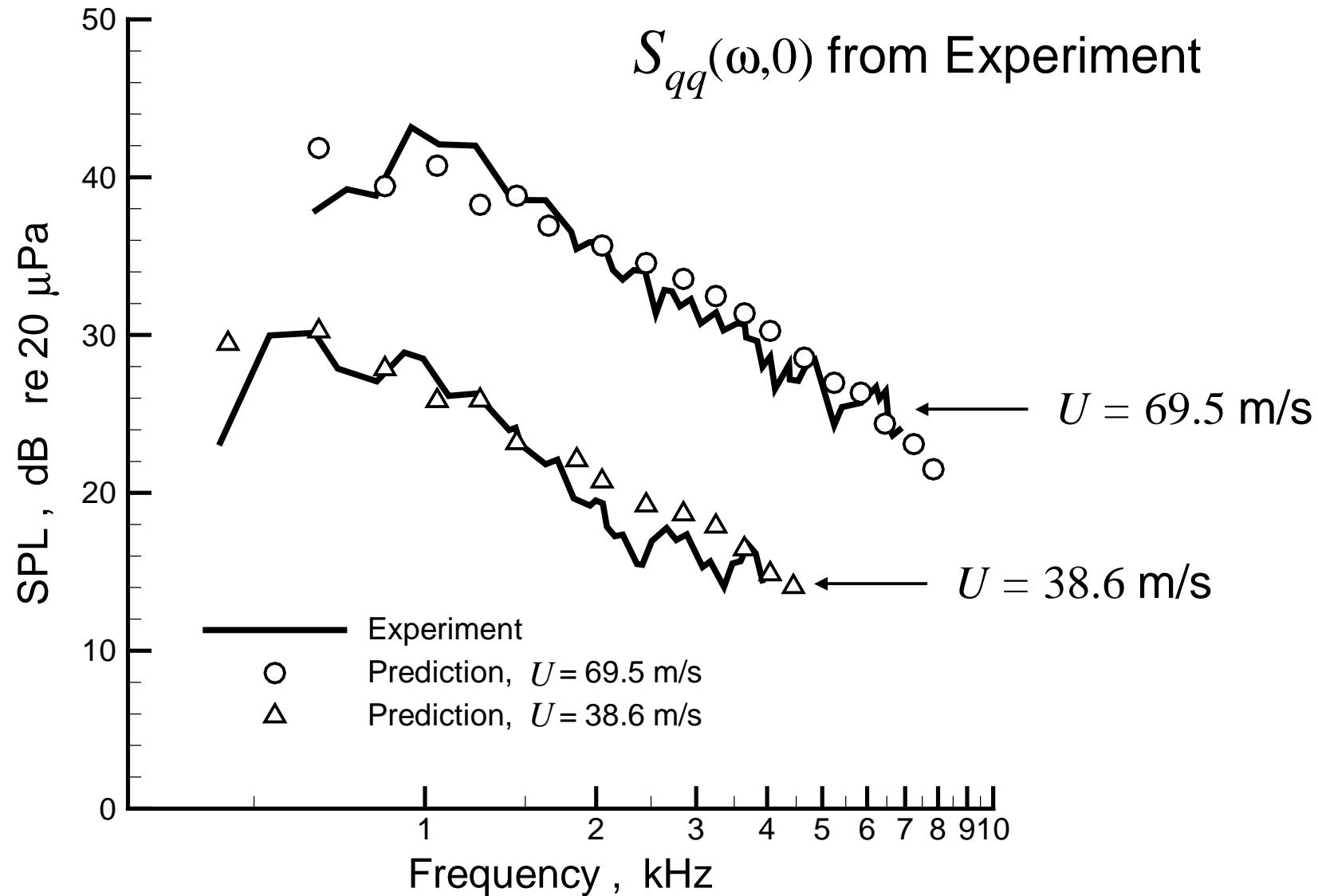


# Surface Pressure Correlations





# Far Field Noise Spectrum





# Concluding Remarks

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- First successful broadband TE Noise predictions in the time domain.
  
- A new solution to the FW-H equation
  - Acoustics decoupled from aerodynamics
  - Valid for general surface motion
  - Statistical formulation